Production of Biogas from Palm Oil Mill Effluent at Pilot Scale: Effect of Recycle Sludge

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ABSTRACT

An anaerobic digestion of palm oil mill effluent (POME) for production of biogas was carried out at pilot scale under thermophilic condition. The objective of this research is to maintain short hydraulic retention time (HRT) and high degradation of the POME to biogas by applying recycle sludge. Fresh POME from PTPN IV without further treatment was used as feed. The fermentation process occurred in a digester tank with the type of continuous stirred tank reactor has a volume of 3 m³ equipped with electrical heaters, mixer, insulators, and baffles in it. To create continuous operation, fresh POME was fed intermittently. A series of experiments with and without recycle sludge were conducted with 616 litres palm oil mill effluent/day feed rate, temperature of feed tank 70 °C, digester tank temperature of 55 °C, stirring rate of 37.5 rpm, six days of hydraulic retention time, and 34% of recycle sludge. The result showed that by extending solid retention time in return sludge process where 34% of digested slurry recycled to the digester, improvement of volatile solid (VS) degradation was obtained around 82.83% at HRT of 6 days. Then, chemical oxygen demand (COD) removal efficiency could be reached until 81% by performing recycle sludge.

Keywords: Anaerobic digestion, Biogas, Palm oil mill effluent, Thermophilic, Pilot plant, Recycle sludge

INTRODUCTION

Crude palm oil (CPO) is one of major products in Indonesia. In 2012 Indonesia produced approximately 23.5 million tons of CPO. It makes Indonesia as the largest CPO producer in the world. But in relation with that, the amount of palm oil mill effluent (POME) generated is also bigger, estimated at three times of CPO production. In general, about 675 liter of POME is produced for every tonne of fresh fruit bunches (FFB) processed.
The most common method used to process POME is the open ponding systems include the cooling pond, anaerobic pond, facultative pond, and aerobic pond. This method is a cheap and easy operating system but it has some disadvantages such as requires a long retention time, the need of large areas, bad odor and the release of methane emission to the atmosphere.  

Irvan et al., in 2012 conducted POME conversion into biogas using anaerobic microbes in a 2 liters continuous stirred tank reactor (CSTR) at temperature of 55 °C (thermophilic), closed systems, intermittent, and HRT variation. The results showed that degradation of COD was still less than 80%, at HRT 10 days. In order to improve the COD degradation, they performed similar experiment by recycling the sludge to the digester in the next research. By extending SRT in return sludge process where 25% of digested slurry recycled to the digester, improvement of volatile solid (VS) degradation was obtained around 84% at HRT of 6 days and SRT of 21 days. Then, chemical oxygen demand (COD) removal efficiency could be reached until 85% by performing recycle sludge. In 2016, Irvan et al., has scaled up the process from laboratory scale to pilot scale, they reported the performance of the two different scales under the same conditions and same POME. Therefore this research was aimed to study the effect of recycle sludge in the new methane fermentation system capable of maintaining high speed and high degradation of POME to biogas at pilot scale.

MATERIALS AND METHOD

Palm Oil Mill Effluent

As the raw material for the experimental anaerobic digestion observed, a real POME taken from PTPN IV Mill wastewater treatment installation were used. Table 1 summarizes the main chemical and physical properties of POME.

Table 1: Properties of POME from PTPN IV Mill

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Unit</th>
<th>Values</th>
</tr>
</thead>
<tbody>
<tr>
<td>Total solid</td>
<td>mg/L</td>
<td>65,000</td>
</tr>
<tr>
<td>Volatile solid</td>
<td>mg/L</td>
<td>54,000</td>
</tr>
<tr>
<td>Suspended Solid</td>
<td>mg/L</td>
<td>35,000</td>
</tr>
<tr>
<td>BOD</td>
<td>mg/L</td>
<td>60,000</td>
</tr>
<tr>
<td>CODcr</td>
<td>mg/L</td>
<td>100,000</td>
</tr>
<tr>
<td>TOD</td>
<td>mg/L</td>
<td>75,000</td>
</tr>
<tr>
<td>Kj-N</td>
<td>mg/L</td>
<td>1,200</td>
</tr>
<tr>
<td>NH3-N</td>
<td>mg/L</td>
<td>80</td>
</tr>
<tr>
<td>Oil and grease</td>
<td>mg/L</td>
<td>9,000</td>
</tr>
<tr>
<td>C</td>
<td>wt %</td>
<td>46.5</td>
</tr>
<tr>
<td>H</td>
<td>wt %</td>
<td>6.5</td>
</tr>
<tr>
<td>N</td>
<td>wt %</td>
<td>2.2</td>
</tr>
<tr>
<td>S</td>
<td>wt %</td>
<td>0.43</td>
</tr>
<tr>
<td>P</td>
<td>wt %</td>
<td>-</td>
</tr>
<tr>
<td>COD : N : P</td>
<td></td>
<td>350 : 4.5 : 0.85</td>
</tr>
<tr>
<td>Carbohydrate</td>
<td>wt %</td>
<td>58.5</td>
</tr>
<tr>
<td>Glucose</td>
<td>wt %</td>
<td>47.5</td>
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<tr>
<td>Cellulose</td>
<td>wt %</td>
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<tr>
<td>Hemicellulose</td>
<td>wt %</td>
<td>0.0</td>
</tr>
<tr>
<td>Lignin</td>
<td>wt %</td>
<td>4.5</td>
</tr>
<tr>
<td>Protein</td>
<td>wt %</td>
<td>11.0</td>
</tr>
<tr>
<td>Lipid</td>
<td>wt %</td>
<td>14.0</td>
</tr>
</tbody>
</table>

Pilot scale of anaerobic treatment of POME

The pilot scale plant was located at a Centre of Community Service of Universitas Sumatera Utara. Fig. 1 shows the flow sheet of the pilot plant. The pilot plant consists of main equipment such as the mixture tank, biogas digester, gas storage, compressor, and biogas generator set. There are two main units include in this process, namely the biogas production unit and the power plant unit. The biogas production unit is a unit that converts POME to biogas. Meanwhile, the power plant unit is a unit that converts biogas into electricity.

The biogas production unit consists of several main equipments: 1,000 litres of feed tank, 3,700 litres of digester tank, 160 litres of mixer tank, 260 litres of gravity thickener, biogas catcher tank equipped with 2,800 litres rubber balloon, a compressor and high pressure biogas tank. The power plant was equipped by engine drive and generator. Engine drive is the used engine of Daihatsu car. Originally, a propulsion engine is a...
gasoline engine-modified fuel so it can use biogas as fuel. While, the electrical generator is a 3 phase motor with a capacity of 12 kWh. Produced gases were then flown into the water trap to collect the unexpected water in the biogas. The flow of the produced biogas was measured by using gas meter. Biogas were sucked by compressor then flown to the generator set to generate the electricity.

EXPERIMENTAL METHOD

Experiments were performed in two methods: with and without recycle sludge. Mass balance of recycle sludge in the continuous stirred tank reactor (CSTR) was analyzed in previous study. Loading up was carried out based on the increased production of biogas which measured by using a wet gas meter (SHINAGAWA, Model W-NK-0.5B). Hydraulic retention time (HRT) of both methods was maintained at 6 days. If biogas production raised by 20%, then the loading up was increased by 20% as well, until HRT 6 days was achieved.

Digested slurry was allowed to settle in a 260 liters of gravity thickener before 34% of it was recycled to the digester. After that, the recycled sludge was analyzed by chemical oxygen demand (COD), total solid (TS), volatile solid (VS), alkalinity, and pH. Concentrations of H₂S and CO₂ in the biogas were measured by using a suction gas injector (GASTEC, type GV-100S) and inspection tube (GASTEC, 25 ~ 1600 ppm).

RESULTS AND DISCUSSIONS

Biogas production in anaerobic fermentation process with and without recycle sludge

Biogas production in the anaerobic fermentation process without recycle sludge needs to be compared with recycle sludge process to see the increase of biogas production due to recycle sludge. For this purpose, experiment of POME fermentation on pilot scale with 616 L/day feed rate, feed temperature at 70 °C feed tank, 55 °C digester temperature, stirring rate 37.5 rpm, HRT target 6 days and recycle sludge 34% was performed. The biogas production rate per mg VS degraded for POME fermentation both with recycle sludge and without recycle are presented in Figure. 2.

During the observation for non-recycle sludge system, it was obtained that the production rate of biogas per mg VS degraded fluctuated. At the beginning of the fermentation, biogas began to increase but at the end of the fermentation period the gas progressively stable. For fermentation without recycle, biogas production rate ranged from 0.0006 to 0.0013 L/mgVS days.
The similar trend is shown by the graph for fermentation with recycle sludge, at first gas production in recycle sludge is slightly higher than that produced by non recycle sludge. For fermentation with recycle sludge, biogas production rate ranged from 0.0005 to 0.0014 L/mgVS days. The same results are also shown by previous study at laboratory scale, where the recycle sludge does not have a significant effect on biogas production.

As shown in Fig. 2, for fermentation with recycle sludge the gas starts to rise slowly until it reaches a stable condition on day 43. However, after a stable period of gas production achieved, it starts to decrease. This is due to the recycle of sludge continuously into the digester, so that the ammonium content in the digester is increased due to the addition of ammonium bicarbonate (NH₄HCO₃). The ammonium content allowed in the digester is a maximum of 200 mg/L. However, in this study the ammonium concentration contained in the reactor was 300 mg/L. Excess value of high ammonium in the digester can be toxic to microbes so that microbial performance becomes ineffective. Biogas production rate ranged from 0.0005 to 0.0015 L/mgVS days.

**Fig. 2. Biogas production in the anaerobic digester with and without recycle sludge**

**Effect of Recycle Sludge on M-alkalinity and pH**

POME obtained from PTPN IV was acidic with pH ranged 3.9 – 4.6. For effective anaerobic digestion process, alkalinity values should range between 2,000 to 5,000 mg/L. This range is intended to neutralize volatile acids (VS) and also to maintain the pH change, which should range between 6.8 – 8.5. In order to maintain to these ranges, additional substance such as sodium bicarbonate (NaHCO₃) was put into the digester. In the feed preparation of this experiment, 2.5 g/l of NaHCO₃ was added to the fresh POME. The pH in the digester with recycle sludge increased to 7.5 from an initial value of 4.0. While, pH in the digester without recycle sludge increased from 4.0 to 7.7. The effect of recycle sludge on M-alkalinity POME fermentation process both with recycle sludge and without recycle are shown in Figure 3.

Alkalinity in the digester without recycle sludge was lower than with recycle sludge. This is due to the sludge which recycled into the digester has high concentration of bicarbonate, whereas the addition of NaHCO₃ in the fresh POME was still performed, so that the bicarbonate accumulated in the digester. From the experimental results, the
alkalinity range of fermentation with recycle sludge is in the range 3,000-5,000 mg/L, which is still within the optimum range for the bacteria working effectively between 2,000 – 5,000 mg/L.

As for fermentation without recycle, pH ranged 7.50 to 8.46. The fermentation pH with or without recycle sludge is in the range of pH allowed for anaerobic fermentation to produce methane gas, between 6.8 - 8.5. The pH in recycle sludge is more stable than non recycle, the fluctuation of pH refers to the microbial conditions present in the digester.

Figure 4 shows the effect of recycle sludge on pH digester, it can be seen that the fermentation with recycle sludge, pH ranged from 7.32 to 7.70.
Alkalinity of the wastewater has a relationship to the pH, if the alkalinity of the waste is high, then the pH will also increase. However, the graph obtained on Fig. 4 has unsuitable relationship where the high alkalinity is on the fermentation with recycle but high pH is in fermentation without recycle. This is due to the fermentation with recycle sludge has higher acidity level by the accumulation of acids formed due to sludge recovery.

**Effect of Recycle Sludge on Total Solid and Volatile Solid**

Changes in the amount of TS and VS values during the anaerobic fermentation process with recycle sludge need to be compared with the process without recycle to see the change in the amount of TS and VS due to recycle sludge. The effect of recycle sludge on changes in TS and VS values in POME fermentation process both with and without recycle is presented in Figure 5.

![Graphs showing total solid and volatile solid profiles](image.png)

**Fig. 5. Effect of recycle sludge on total solid and volatile solid**
As shown in Fig. 5, in the fermentation without recycle sludge, TS decreased from 29,700 mg/L to about 19,800 mg/L, then relatively constant at 20,000 mg/L. While, with recycle sludge TS relatively constant at value range 21,000 – 28,000 mg/L. TS in the digester with recycle sludge was higher than without recycle, this is because the sludge recycled to the digester came from the bottom of the gravity thickener that are still containing material with high TS. A similar profile is also shown for VS, where VS in the digester with recycle sludge was higher than without recycle. This occurs because the recycle of organic materials are degraded more than fermentation without recycle.

**Effect of Recycle Sludge on VS Degradation Rate**

The effect of recycle sludge on the rate of VS degradation in POME fermentation process with and without recycle sludge is shown in Figure 6.

![Graph showing the effect of recycle sludge on VS degradation](image1)

**Fig. 6. Effect of recycle sludge on VS degradation**

![Bar chart showing the effect of recycle sludge on COD degradation](image2)

**Fig. 7. Effect of recycle sludge on COD degradation**
As shown in Fig. 6, in the fermentation process without recycle sludge at HRT 6 days, VS degradation had the highest value of 65% and the lowest value of 48.6%. While in the fermentation process with recycle sludge, due to the increase of solid retention time, VS degradation reached maximum value at 82.8 %, while the lowest value of 59% was achieved. In other words, the longer sludge time in the reactor increases the degradation rate at the same HRT by recycling the sludge into the digester. It can be concluded that fermentation with recycle sludge has better performance than fermentation without recycle. Similar results were also obtained in previous study at laboratory scale7.

**Effect of Recycle Sludge on COD Removal**

Many parameters have been used to measure the efficiency of an anaerobic process in terms of quality and quantity of biogas produced, however we still need the parameter that serve as an indicator to measure the quality of the liquid waste discharged from the digester which are also very important and should take into account for the standard quality of applicable industrial effluent. The most commonly used parameter in this case is COD (chemical oxygen demand), which is the indirect measure of the number of organic compounds, both biodegradable and non-biodegradable.

Figure. 7 shows the effect of recycle sludge on COD degradation. At HRT 6 days, fermentation of POME to biogas using recycle sludge, COD removal efficiency was 81%, while using non recycle sludge COD removal efficiency was only 76 %. This proves that the fermentation with recycle sludge can increase the COD removal in anaerobic process. This was confirmed by previous researchers who have demonstrated that COD removal efficiency in the fermentation with recycle sludge was lower than fermentation without recycle sludge11-13.

**CONCLUSIONS**

This study has demonstrated the feasibility of anaerobic digestion of POME with recycle sludge at pilot scale. During the fermentation with recycle sludge, biogas generation was decreased due to the increasing of ammonium content. Alkalinity, TS, VS, and VS degradation in the digester with recycle was higher than without recycle sludge. In the same HRT, degradation rate of COD in fermentation with recycle was higher than without recycle, 81% and 76%, respectively.

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